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Design Calculations For Soft X-Ray
Electron Temperature Diagnostic System

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A B S T R A C T

X-Rays emitted by a hot plasma are used for determination of electron temperature. This diagnostics is useful when electron temperature is above 100 eV and electron - ion densities are high enough ($\geq 10^{12} - 10^{13} \text{ cm}^{-3}$) to produce detectable X-Ray flux. Some relevant aspects of the radiation from a hot plasma are briefly discussed. The X-Ray transmission ratio technique is discussed in detail. Calculations for selecting suitable components for such a diagnostic system are presented in this note. Ratios of the transmitted X-Ray flux through different sets of beryllium and aluminium foils, as a function of electron temperature are calculated. Some aspects of the method of determining electron temperature from the pulse height analysis of the emitted X-Ray spectrum are discussed briefly.

1) Introduction

X-Ray diagnostics is now a well established technique for determination of electron temperature (kT_e) in hot plasmas, where $kT_e > 100$ eV. Many papers and reports on this diagnostics have appeared so far.¹⁻⁸⁾ The purpose of this report is to present some calculations essential for an experimentalist to design the diagnostic system. These calculations will be helpful in selecting the suitable detector components in a particular experiment. These calculations assume the knowledge of the expected values of electron temperature and density in the heated plasma. These values can be calculated knowing the energy input in the plasma, for heating, and the energy balance considerations. Basic principles involved in this diagnostics are well discussed in the reports mentioned earlier, and we, therefore, avoid repetition.

2) Radiation from Plasma

The radiation emitted by a plasma extends over the entire electromagnetic spectrum. There are three radiation processes in an unmagnetized plasma, viz. (i) free-free or bremsstrahlung (ii) free-bound or recombination and (iii) bound-bound or line radiation. If the atoms composing the plasma are of atomic number Z , the free-free radiation will dominate for $kT_e > 3.V_H.Z^2$, where V_H is the ionization potential of hydrogen ($= 13.6$ eV). The recombination process will be effective at lower temperatures. It is to be noted that the

Intensity of f-f, f-b and b-b radiations are proportional Z^2 , Z^4 and Z^6 respectively. In most of the plasma heating experiments hydrogen ($Z = 1$) plasma is used. Impurities of high Z values (mainly of oxygen), give rise to line radiation. Presence of f-b and b-b radiations complicates the diagnostics. Since the line radiations from impurities are at higher wavelengths, it can be eliminated by using suitable absorber foils. In this report we will consider only the free-free radiation process.

Bremsstrahlung

This type of radiation arises from the interaction of electrons with the positive ions in the plasma. In this process a free electron makes a transition to another free state of lower energy, with the emission of a photon. The spectrum is continuous. Assuming the plasma electrons to follow Maxwellian distribution, the intensity of free-free radiation per Angstrom is given by¹⁾

$$= 1.9 \times 10^{-28} N_e N_i Z^2 g (kT_e)^{-1/2} \lambda^{-2} \exp \left[\frac{hc}{\lambda kT_e} \right] \frac{\text{Watt}}{\text{cm}^3 \cdot \text{\AA}} \dots (1)$$

In this equation N_e and N_i are the electron and ion densities (m^{-3}) respectively, Z is the atomic number of atoms composing the plasma, g is the Gaunt factor, kT_e is the electron temperature in eV, λ is the wavelength in \AA of the emitted X-Ray radiation, h is Plank's constant and c is the velocity of light. In our calculations we will assume $g = 1$, significance which has been discussed by Elton⁴⁾. In the exponential

term, hc/λ is the energy E_λ , of the photon corresponding to wavelength λ . ($E_\lambda = \frac{12.4}{\lambda} \text{ KeV.}$) When I_λ is plotted as function of λ , for a given value of kT_e , I_λ is maximum at a wavelength given by $\lambda_{\max} = \frac{6200}{kT_e} \text{ \AA}$. Variation of I_λ with λ for different values of kT_e , for an arbitrary value of $N_e = N_i = 10^{14} \text{ cm}^{-3}$ were calculated using Eq.(1) and are plotted in Fig.1. These curves show that the short wave length (high energy) cut-off depends on kT_e . In the wavelength region $\lambda \gg \lambda_{\max}$, the spectrum is not affected by the change in kT_e . The strong dependence of the high energy cut-off of the spectrum on kT_e , is used as the basis for measuring kT_e in hot plasma. Spectral measurements for this purpose should be made in the region $\lambda < \lambda_{\max}$, where the spectrum strongly depends on kT_e . This diagnostics can be used only when λ_{\max} is in X-Ray region and electron density is high enough ($> 10^{13} \text{ cm}^{-3}$) to produce detectable flux of X-Ray photons. Integration of Eq.(1), over 1 to 100 \AA gives the power emitted by the unit volume of plasma in the soft X-Ray region, which is equal to

$$1.9 \times 10^{-28} N_e N_i Z^2 (kT_e)^{-\frac{1}{2}} \int_1^{100} \lambda^{-2} \exp\left[-\frac{hc}{\lambda \cdot kT_e}\right] d\lambda. \quad \dots (2)$$

This X-Ray emission from the plasma is isotropic i.e. uniform over the solid angle of 4π .

As the electron temperature increases, fraction of the power emitted in the lower wavelength region increases.

Diagnostics

For determination of electron temperature from the γ measurements, two different methods are available. In first method, the intensities of X-Rays transmitted through different metallic absorber foils of known thickness are measured¹⁾. Thin foils of beryllium and aluminium are generally used. By knowing the ratio of the transmitted intensities through two foils of different thickness, electron temperature can be determined. The experimental arrangement for this technique is shown in Fig.2. In the second method, the X-Ray photon spectrum is recorded by a multichannel pulse height analyser^{9,10)}. Electron temperature is then determined from slope of the differential photon spectrum. Further details of these methods are discussed in sections 9 and 10 respectively.

In most of the plasma heating experiments the plasma is in the high energy state, when the measurable X-Ray emission takes place, for about few microseconds or less. Fast detectors are to be used for measuring X-Rays from such plasmas. The Scintillator - Photomultiplier combination is mostly used for measuring X-Ray flux, in both the above mentioned methods. In the next three sections, calculations required for selecting suitable absorber foils, scintillator thickness and photomultiplier tube are given.

Selection of absorber foils

When a polychromatic beam of X-Rays (containing photons

of a wide energy range) passes through an absorber, the low energy photons are absorbed in it and the beam intensity is attenuated. For selecting suitable absorber thickness, the photon energies which will be cut-off (intensity attenuated to one tenth of original) by various foil thicknesses should be known. These cut-off energies for known thicknesses of different materials can be calculated as follows.

Let I_0 is the intensity of a monochromatic X-Ray beam, passing through an absorber of thickness t (cm). Intensity of the transmitted beam is given by¹¹⁾

$$I = I_0 \cdot \text{Exp} (- \rho \cdot K_\lambda \cdot t) \dots\dots\dots (3)$$

In the above equation, ρ is the density of absorber material (gm/cm^3) and K_λ is the mass absorption coefficient (cm^2/gm), which depends on absorber material and wavelength of X-Rays. For a given absorber of thickness T (cm), the required value of K_λ to attenuate a beam of energy E_c to one tenth of its original intensity is given by

$$\begin{aligned} \ln 10 &= \rho \cdot K_\lambda T, \\ \text{or } K_\lambda &= \ln 10 / \rho T \dots\dots\dots (4) \end{aligned}$$

Variation of K_λ with wavelength is known for most of the elements. For a given substance, the wavelength λ_c , corresponding to the value of K_λ given by Eq.(4) can be determined. Thus, the energy E_c of the beam corresponding to this wavelength, which will be cut-off by the foil of thickness T (cm) can be determined. For approximate calculations of E_c , the empirical relations between K_λ and λ can

sed. This empirical relation is

$$K_{\lambda} = C (\lambda)^n,$$

where C and n are constants depending on the atomic number of the absorber material, and can be calculated easily. Thus, the relation can be written as

$$\lambda_c = \left[\frac{\ln 10}{C \rho T} \right]^{1/n} \text{ \AA}$$

$$E_c = \frac{12.4}{\lambda_c} \text{ KeV}$$

For beryllium, $\rho = 1.8 \text{ gm/cm}^3$; $C = 0.3731$, $n = 2.901$ for 107 \AA (K absorption edge); for aluminium $\rho = 2.7 \text{ gm/cm}^3$, $C = 13.9292$, $n = 2.8469$ for $\lambda < 7.9 \text{ \AA}$. Using these values, the cut off energies were calculated for aluminium and beryllium and are given in Table 1. Values of the cut off energies can also be calculated by using Eq.(4) and the experimentally determined values of K_{λ} . Calculated values of E_c for aluminium and beryllium using the values of K_{λ} given in ref. (11) were found to be almost equal to those calculated using the empirical relation mentioned above.

Transmitted intensity and Scintillator

The intensity I_{λ} at any wavelength λ , transmitted through an absorbing foil of thickness $D \text{ mg/cm}^2$ ($t = t \cdot \rho \cdot 1000$) and mass absorption coefficient K_{λ} is calculated from Eq.(1)

(3) to be

$$I_{\lambda} = 1.9 \times 10^{-28} N_e N_i Z^2 (kT_e)^{-1/2} \lambda^{-2} e^{-\rho \left(\frac{hc}{\lambda kT_e} - K_{\lambda} \cdot D \right)} \dots (5)$$

The total flux transmitted through a given foil can be calculated by integrating Eq.(5) over a wavelength region. The transmitted X-Rays fall on the scintillator. Plastic scintillators NE102 and NE140 (manufactured by Nuclear Enterprises Ltd) are the typical scintillators used. These scintillators have sufficient response for photon energy as low as 1 keV. The NaI crystals can not be used below 3 keV¹¹⁾. For efficient working of the scintillator, i.e. to get maximum light output in visible range, photons with all energies in the transmitted signal should be completely absorbed in it. Knowing the expected upper limit of X-Ray photon energy, the required thickness of scintillator can be calculated. As an example, calculations for determining the required thickness of NE 102 for 90% absorption of 10 KeV photons are given here. This scintillator contains 4.78×10^{22} carbon atoms/cm³ and 5.28×10^{22} hydrogen atoms/cm³ as specified in its manufacturers catalogue. Using Avagadro number and atomic weights of carbon and hydrogen, it is seen that NE 102 contains 0.953 gm of carbon/cm³ and 0.088 gm of hydrogen/cm³. Using the formula for the mass absorption coefficient of a compound¹¹⁾, and using the values of absorption coefficients of carbon and hydrogen at 10 KeV (0.12 \AA) given by Victoreen,¹²⁾ it is found that the mass absorption coefficient of NE 102 for 10 KeV photons is $1.93 \text{ cm}^2/\text{gm}$. Again using Eq.(4), the required thickness of NE 102 is found to be 1.04 cm. It is advisable to use the scintillator thickness slightly more than the calculated. Proceeding in this way, the required thickness

any scintillator of known composition can be calculated.

Photomultiplier Tube

Selection of the photomultiplier tube (PMT) is to be made considering the spectral distribution of the scintillator light output. For example, the light output of NE102 scintillator is distributed over the range of 4000 to 5000 Å, with maximum emission at 4230 Å. The PMT should be with the photocathode of maximum response very near to 4230 Å. Photomultiplier tubes with S-11 spectral response with a maximum sensitivity at 4400 Å are generally used with NE 102. PMT of the required spectral response and diameter permitted by the experimental geometry should be selected. The scintillator and PMT should be in perfect optical contact, so that maximum number of photons from the scintillator fall on the photocathode of the PMT.

Number of Photons

The number of photons emitted by the plasma and those transmitted through an absorber foil of known thickness should also be known. Particularly, for using the method of multichannel analysis mentioned in sec.4, the number of photons emitted between small energy intervals should be known in order to select a suitable analyser.

Expression for the number of photons emitted by the plasma, can be derived from Eq.(1). Energy emitted between wavelengths λ and $\lambda + d\lambda$ due to free-free radiation is given by

$$I_{\lambda} d\lambda = 1.9 \times 10^{-28} N_e N_i Z^2 (kT_e)^{-1/2} \lambda^{-2} \exp\left[-\frac{E_{\lambda}}{kT_e}\right] \frac{\text{Watt}}{\text{cm}^3}$$

OR

$$I_{\lambda} d\lambda = 1.9 \times 10^{-28} \times 6.24 \times 10^{18} N_e N_i Z^2 (kT_e)^{-1/2} \lambda^{-2} \exp\left[\frac{-E}{kT_e}\right] \frac{\text{eV}}{\text{Sec.cm}^3} \quad (6)$$

We have the relation

$$E_{\lambda} = \frac{12400}{\lambda} \text{ eV}$$

$$\text{or } dE_{\lambda} = -12400 \lambda^{-2} d\lambda \quad \dots \quad (7)$$

Number of photons emitted within energy E_{λ} and $E_{\lambda} + dE_{\lambda}$ is now given by

$$dN = \frac{I_{\lambda} d\lambda \text{ (eV)}}{E_{\lambda} \text{ (eV)}}$$

$$\text{or } dN = 1.9 \times 6.24 \times 10^{-10} N_e N_i Z^2 (kT_e)^{-1/2} \frac{1}{E} \lambda^{-2} \exp\left(\frac{-E}{kT_e}\right) d\lambda$$

Using relation (7), we get

$$dN = 9.56 \times 10^{-14} N_e N_i Z^2 (kT_e)^{-1/2} \frac{1}{E} \exp\left(-\frac{E}{kT_e}\right) dE \frac{\text{Photons}}{\text{sec.cm}^3 \cdot \text{eV}} \quad (8)$$

Using above expression, the number of photons emitted by the plasma in given energy interval can be calculated. To get the number of photons from unit plasma volume emitted in unit solid angle, Eq.(8) is to be divided by 4π . Number of photons passing through an absorber of thickness D (mg/cm^2) and between energy E and $E + dE$ can be written from equns. (8) and (3) as

$$dN = 9.56 \times 10^{-14} N_e N_i Z^2 (kT_e)^{-1/2} \frac{1}{E} \exp\left(-\frac{E}{kT_e} - K_E D\right) dE \dots \quad (9)$$

In above expression, K_E is the mass absorption coefficient as a function of photon energy.

9) Transmission Ratio Technique

As mentioned in sec. (4), further details of the

mission ratio technique are discussed here. Knowing expected values of kT_e and N_e , the expected X-Ray spectrum can be plotted using Eq.(1), and λ_{max} can be determined. For selecting the absorber thickness, the dependence of only the high energy side of the spectrum on foil thickness should be remembered. Foil thickness with cut-off energy greater than $\frac{12.4}{\lambda_{max}}$ KeV, and with sufficient intermediate gap (of 1 KeV) should be selected. Consideration for selecting the scintillator and photomultiplier are already discussed in secs. 6 and 7. Signal of the photomultiplier amplified by suitable preamplifier, amplifiers and finally recorded on an oscilloscope.

For actual design of the X-Ray detector, the plasma geometry and relative position of detector are to be considered. Solid angle ω subtended at the scintillator should be calculated. This solid angle gives the volume of the plasma seen by the detector. Multiplying Eq.(5) by the plasma volume seen by the detector, life time of heated plasma and $\omega/4\pi$, we get the transmitted flux. In plasma heating experiments, when the plasma parameters are to be determined one shot, the transmitted X-Ray flux through two or more absorbers are to be measured in one shot. In this situation, photomultiplier tubes can be placed in one diagnostic port, and using two ports, flux transmitted through four absorbers can be measured in one shot. An alternative arrangement using light guides in one port, is described by

Ratio of the integrated X-Rays transmitted through absorber, to the total incident X-Ray flux is to be calculated for different absorbers, for determining kT_e . This ratio can be written from Eq.(1) and (5) as

$$\frac{\int \lambda^{-2} \exp \left[- \frac{hc}{kT_e} - K_\lambda \cdot D \right] d\lambda}{\int \lambda^{-2} \exp \left[- \frac{hc}{kT_e} \right] d\lambda}, \dots \quad (10)$$

limits of these integrations depend on the range of kT_e . For values of kT_e of the order of 500 eV, this integration should be done over 1 to 100 Å. At still higher temperatures of the order of 1 KeV and above, the lower limit should be 0.1 Å. This ratio should be calculated for different values of kT_e and the selected values of absorber thickness. This ratio was calculated for beryllium and aluminium foils of different thickness, and its variations with absorber thickness, for different values of kT_e are shown in Fig.3. High purity beryllium foils of thickness ranging between 0.001" and 0.02" are available from Brush Wellman Inc. (17876 St.Clair Avenue, Cleveland, Ohio 44110, USA), and these thicknesses are used in present calculations. These standard thicknesses given in inches have been converted into mg/cm^2 and are given in Table 1 (B). Mass absorption coefficients for beryllium were taken from ref. (14). Aluminium foils of different thickness ranging from 2.7 to 864 mg/cm^2 are available from Electronic Corp. of India Ltd., and some of these standard thicknesses are used in these calculations.

off wavelengths and cut-off energies of aluminium foils available from ECIL were calculated as stated in sec.5 and given in Table 2. Mass absorption coefficients for aluminium were taken from ref. (15). The integrals were numerically calculated using the IBM 360 Computer and the results were automatically plotted by the plotter of the computer system. From these calculations, ratio of the transmitted flux through two selected absorbers, for different values of kT_e were calculated. These results are shown in Fig.4. Thus, using the experimentally obtained values of these ratios, and the curves plotted in Fig.4, kT_e can be determined.

Multichannel Analysis

For finding the suitability of this method, selecting the analyser and number of channels to be used, the number of photons emitted between small energy intervals are to be calculated. A thin filter in the form of metallic foil is used to avoid the ultraviolet and long wavelength radiation. Illustrating these calculations, we take an example of hydrogen plasma in which $kT_e = 500$ eV and $N_e = 10^{14} \text{ cm}^{-3}$. The energy from 0.12 KeV ($\lambda = 100 \text{ \AA}$) to 10 KeV is divided between 100 channels, each channel of width of 0.0988 KeV. Number of photons emitted in these energy channels per unit solid angle were calculated using Eq.(9). The graph between number of photons and the energy interval for the two absorbers is shown in Fig.5. The linear portion of the

The essential condition for using this technique is that, sufficient number of photons should be emitted in each energy channel which can be measured within the statistical error of measurements. In Fig.5, we see that number of photons emitted in the useful energy range is very small and thus, this technique should not be used in present case. This method can be used at still higher temperatures.

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Table 1 - (A) Cut off Wavelengths and Energies for Aluminium Foils

Thickness Inches	Thickness cm	Thickness mg/cm ²	Cut off Wavelength Angstroms	Cut off Energy KeV
0.001	0.00254	6.858	3.058	4.061
0.002	0.00508	13.716	2.397	5.181
0.003	0.00762	20.574	2.079	5.974
0.004	0.01016	27.432	1.879	6.609
0.005	0.01270	34.290	1.738	7.148
0.006	0.01524	41.148	1.630	7.620
0.007	0.01778	48.006	1.544	8.044
0.008	0.02032	54.864	1.473	8.431
0.009	0.02286	61.722	1.413	8.787
0.010	0.02540	68.580	1.362	9.118
0.011	0.02794	75.438	1.317	9.429
0.012	0.03048	82.296	1.278	9.721
0.013	0.03302	89.154	1.242	9.998
0.014	0.03556	96.012	1.210	10.262
0.015	0.03810	102.870	1.181	10.514
0.016	0.04064	109.728	1.155	10.755
0.017	0.04318	116.586	1.130	10.986

Table - 1 (B) Cut-Off Wavelengths and Energies for Beryllium Foils

Thickness inches	Thickness cm	Thickness mg/cm ²	Cut Off Wave- length Angstroms	Cut-Off energy KeV
0.001	0.00254	4.699	11.883	1.045
0.002	0.00508	9.358	9.358	1.327
0.003	0.00762	14.097	8.137	1.526
0.004	0.01016	18.796	7.369	1.685
0.005	0.01270	23.495	6.823	1.820
0.006	0.01524	28.194	6.408	1.938
0.007	0.01778	32.893	6.076	2.044
0.008	0.02032	37.592	5.803	2.140
0.009	0.02286	42.291	5.572	2.229
0.010	0.02540	46.990	5.373	2.312
0.011	0.02794	51.689	5.199	2.389
0.012	0.03048	56.388	5.046	2.461
0.013	0.03302	61.087	4.908	2.530
0.014	0.03556	65.786	4.785	2.596
0.015	0.03810	70.485	4.672	2.658
0.016	0.04064	75.184	4.569	2.718
0.017	0.04318	79.883	4.475	2.775
0.018	0.04572	84.582	4.388	2.831
0.019	0.04826	89.281	4.307	2.884
0.020	0.05080	93.980	4.231	2.935

Table - 2 Aluminium Foils Available from ECIL

S.No.	Thickness in mg/cm ²	Thickness in cm.	Cut-off wavelength in Angstrom	Cut-Off energy in KeV
1	2.7	0.001	4.2428	2.9273
2	5.4	0.002	3.3259	3.7343
3	13.4	0.0049	2.4278	5.1157
4	27.0	0.010	1.8897	6.5724
5	40.5	0.015	1.6389	7.5782
6	84.5	0.0312	1.2671	9.8019
7	219	0.0811	0.9059	13.7101
8	243	0.090	0.8734	14.2202
9	324	0.120	0.7894	15.7334
10	432	0.160	0.7136	17.4047
11	540	0.200	0.6598	18.8238
12	709	0.262	0.6001	20.6965
13	864	0.320	0.5594	22.2023

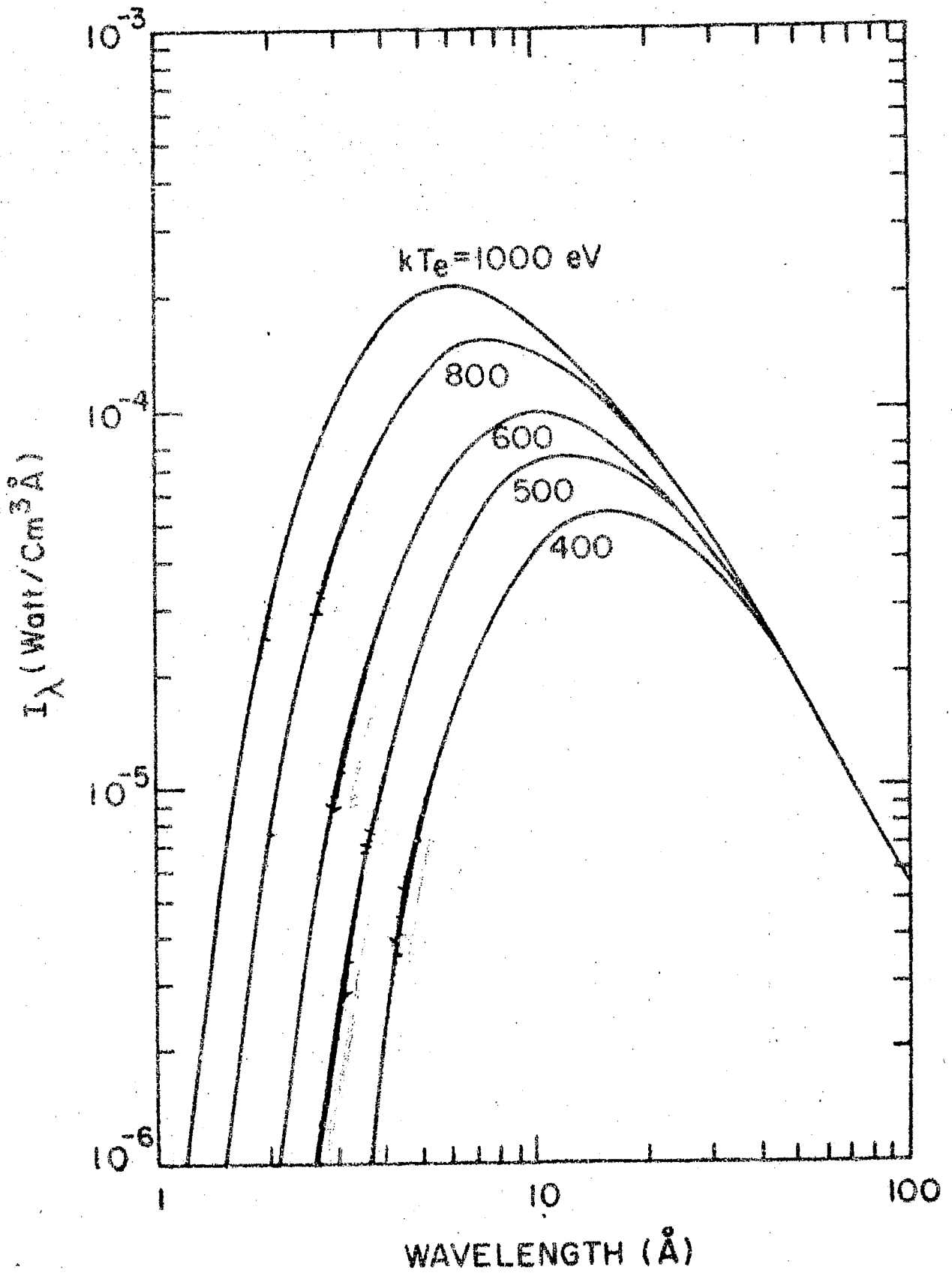
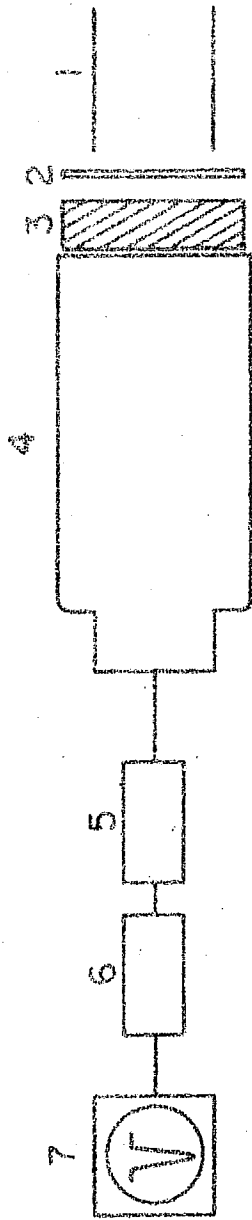


Fig.1. Calculated bremsstrahlung emission per cm³,
for Hydrogen Plasma. $N_e = 10^{14}$ cm⁻³.

X-RAY EMITTING PLASMA



- 1 COLLIMATOR
- 2 ABSORBER FOIL
- 3 SCINTILLATOR
- 4 PHOTO MULTIPLYER TUBE
- 5 PRE AMPLIFIER
- 6 AMPLIFIER
- 7 OSCILLOSCOPE

Fig.2. Experimental arrangement for determination of electron temperature by transmission ratio technique.

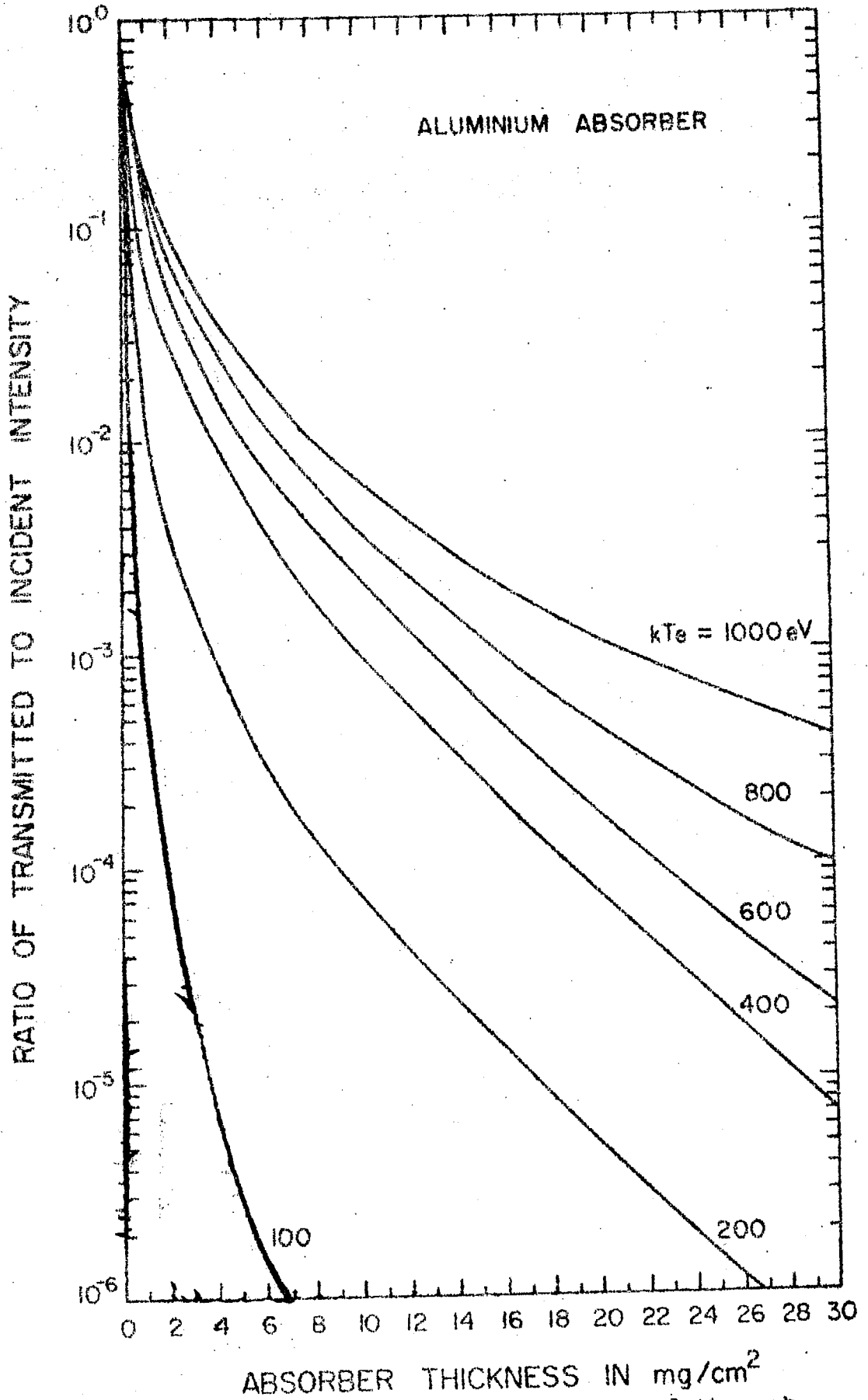


Fig. 3 (a), Ratio of X-Rays transmitted through Aluminium foils to the total incident

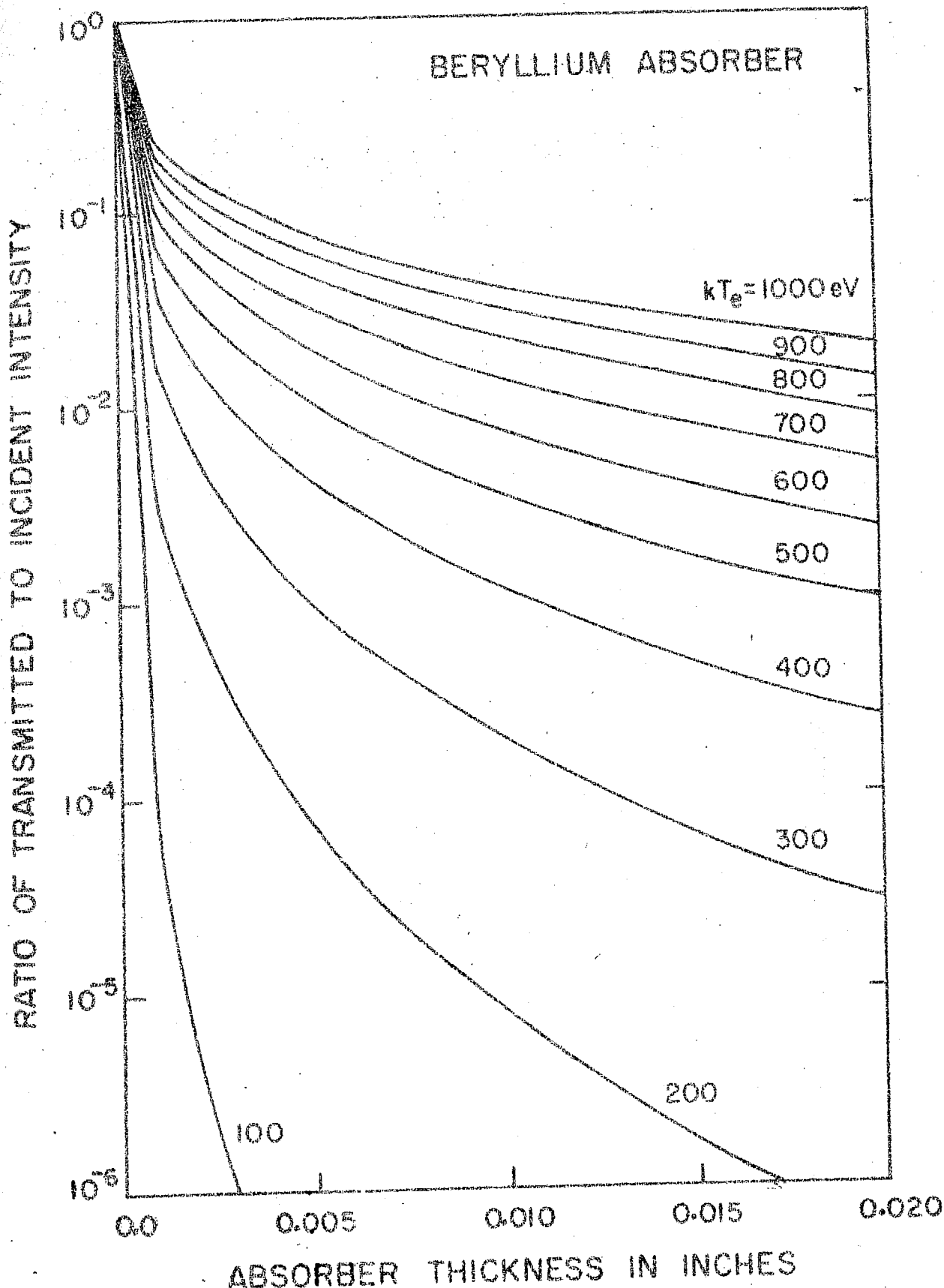


Fig. 3. (b) Ratio of X-Rays transmitted through beryllium foils to the total incident flux versus foil thickness.

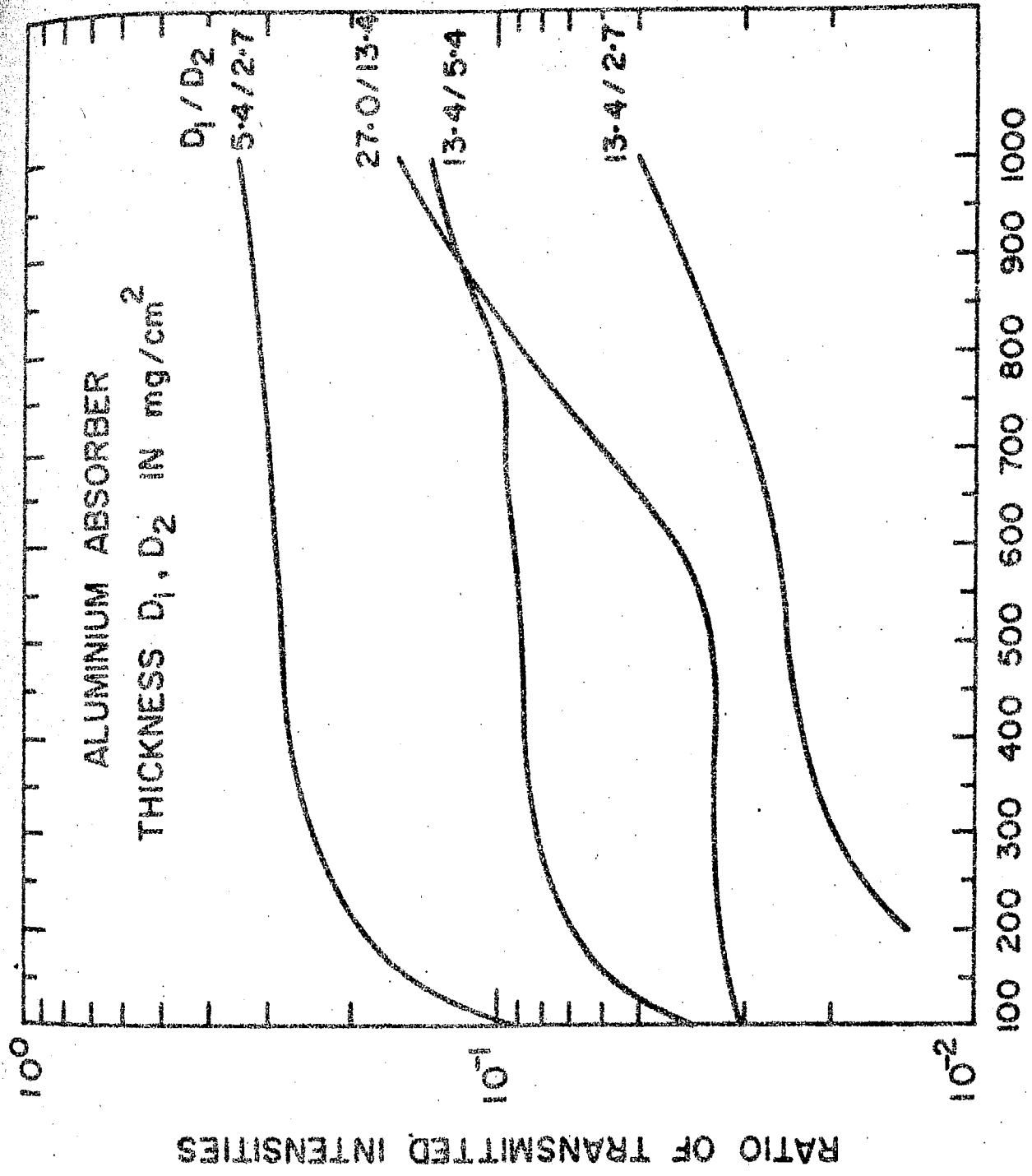


Fig.4 (a). Ratio of transmitted X-Rays through combinations of two aluminium foils versus electron temperature.

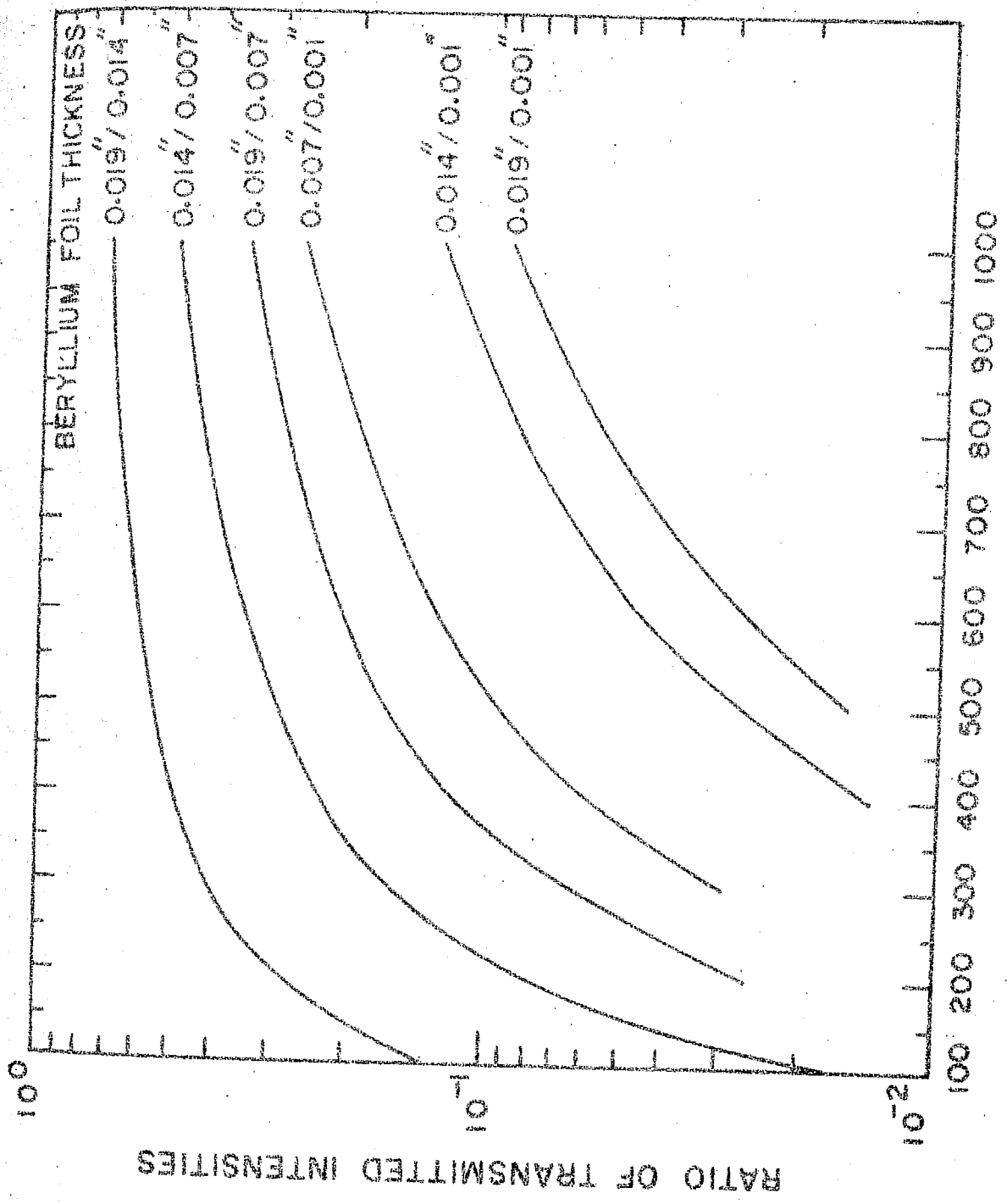


Fig. 4 (b). Ratio of transmitted X-rays through combinations of two beryllium foils versus electron temperature.

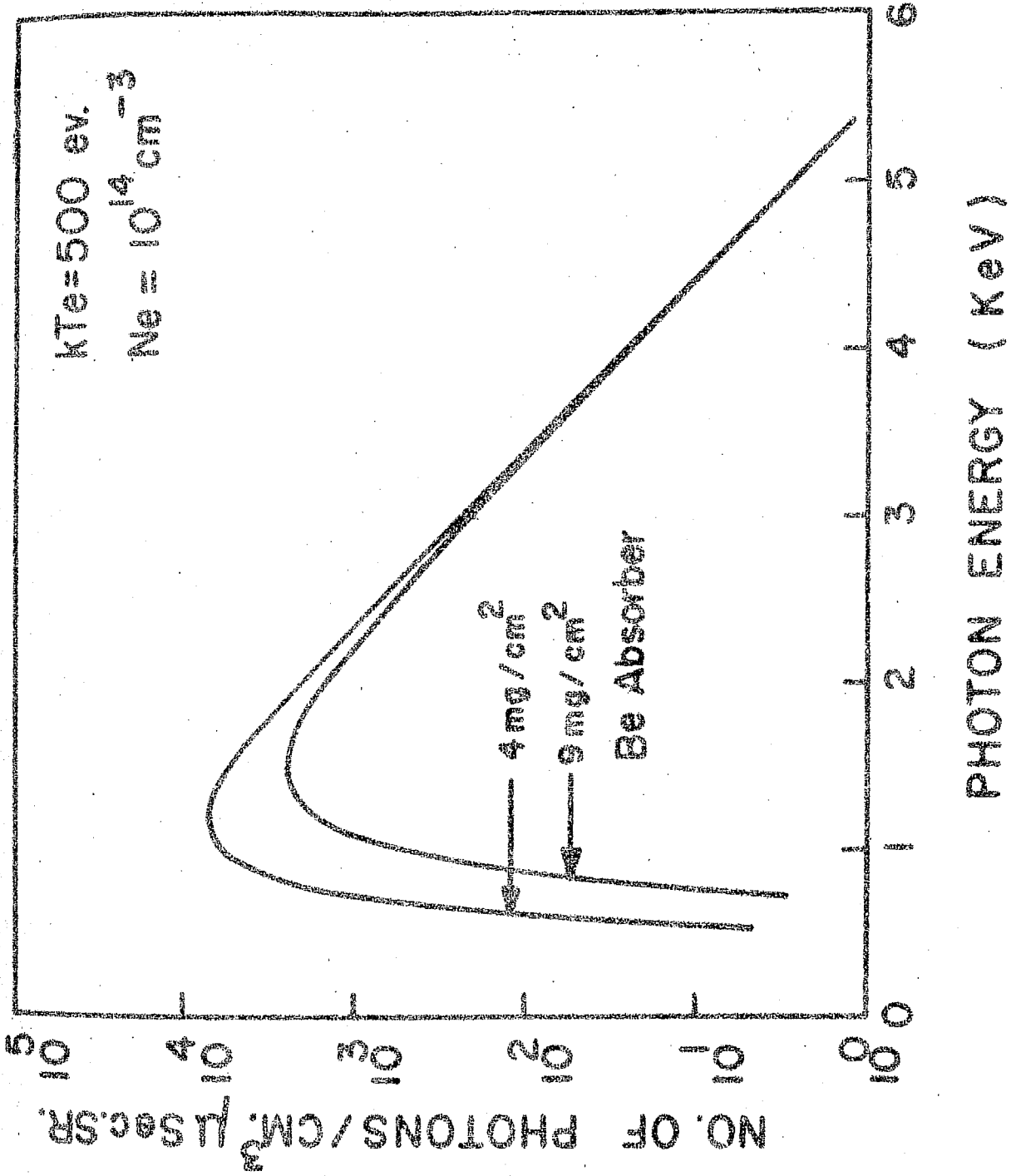


Fig. 5 Calculated photon spectrum